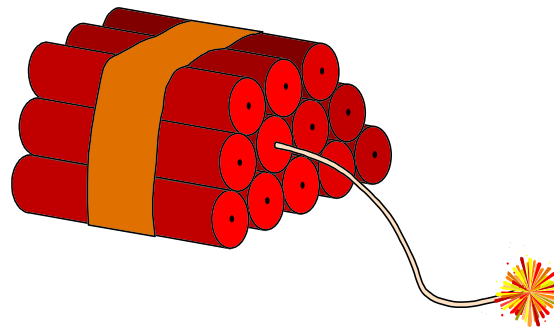


# HE MATERIAL MODELING AND VALIDATION



JOBIE M. GERKEN  
JOEL G. BENNETT  
ESA-EA

# A TRUE TEAM EFFORT

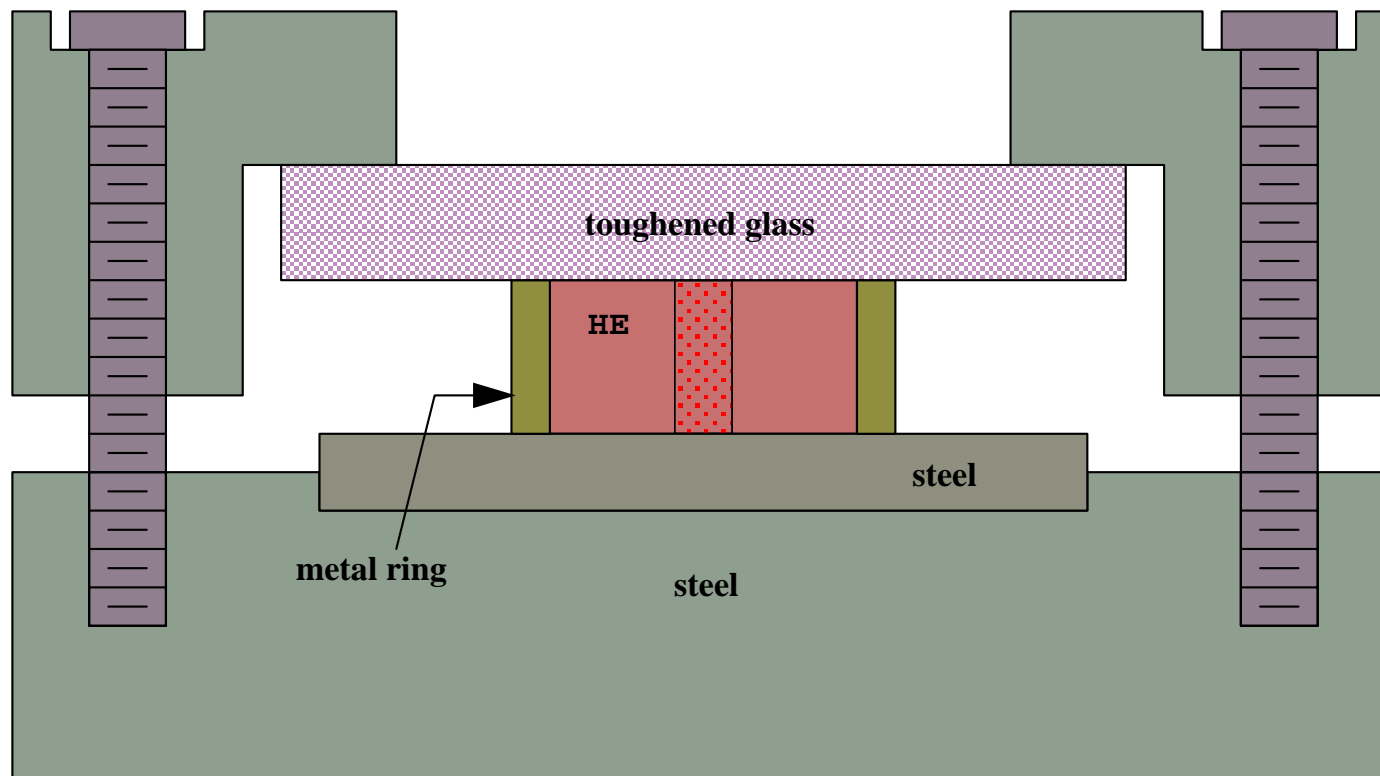
**Frank Addressio T-3**  
**Mike Stout MST-7**  
**Jim Johnson T-7**  
**John Dienes T-14**

**Supported by:**  
**Phil Howe**  
**Joe Repa**  
**George Hurley**

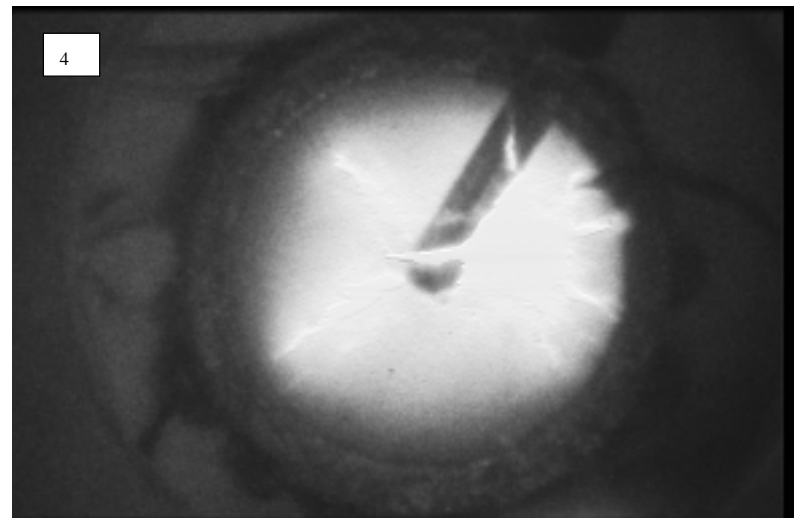
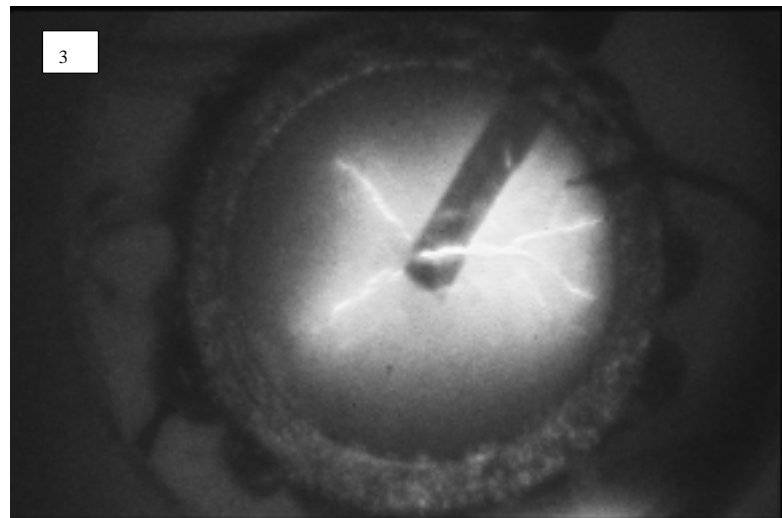
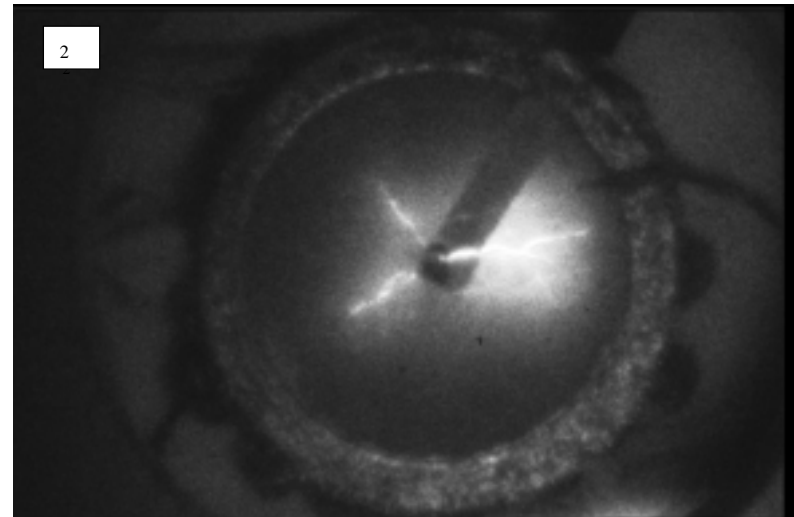
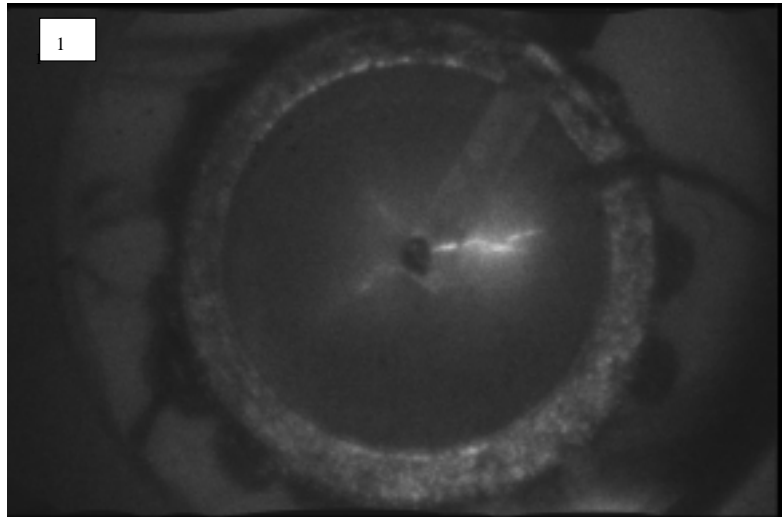
**Joel Bennett ESA-EA**  
**Keith Haberman ESA-EA**  
**Bob Hackett “Ole” Miss.**  
**Fred Smith CSU**

**Blaine Asay DX-2**  
**Deanne Idar DX-2**  
**Colin Sadler DX-2**  
**Cheng Liu MST-7**  
**G.T. “Rusty” Gray MST-8**

# Mechanically Coupled Cook-Off



# Mechanically-Coupled Cookoff Results



# Mechanically Coupled Cookoff

- **An “Engineering Simulation Challenge”**
- **Requires “lots” of tools to come together in the same place, (i.e. in the same code)**
  - **Thermal stress because of heat-up (implies an implicit code capability)**
  - **Discrete cracking model - Gerken/Smith/Bennett**
  - **HE material model (Implicit ViscoSCRAM)**
  - **HE damage cracking model (ViscoSCRAM)**
  - **Bulk thermal heating model (ViscoSCRAM)**
  - **HE ignition model (ViscoSCRAM)**

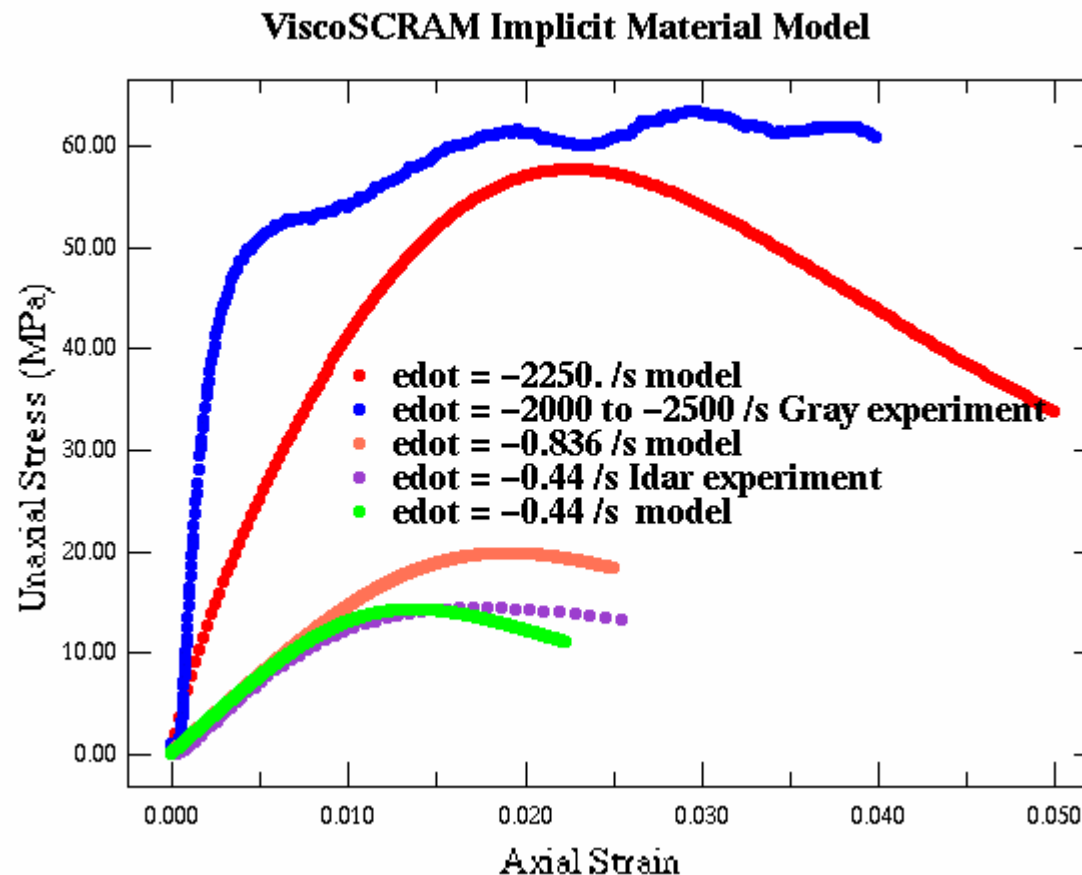
# ViscoSCRAM for PBX 9501

- Viscoelastic material behavior with shear and tensile average crack growth and resulting damage accumulation (SCRAM).
- Bulk thermal heating and frictional hotspot ignition model.
- Implemented in the explicit codes DYNA3D, PRONTO3D, and SHAVANO/KITO and in an implicit form for ABAQUS Standard.

# Validation of ViscoSCRAM

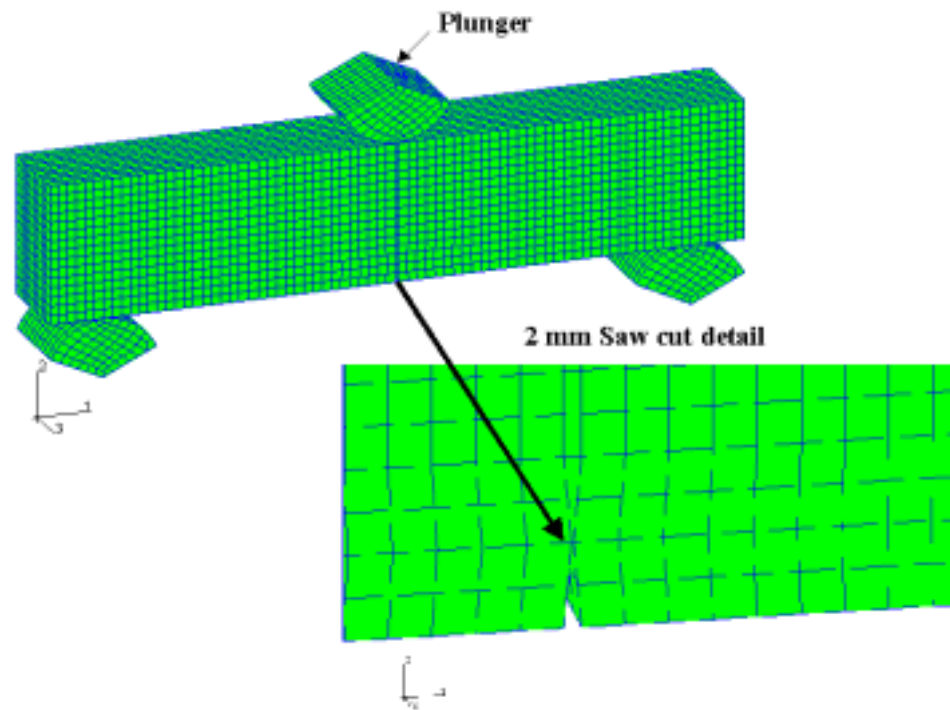
- One Dimensional Compression Tests
  - Low Rate - D. Idar, 0.001 to 0.44 /s tests
  - Higher Rate - G.T. Gray 2000-2500 /s “Hoppy” Bar tests
- Sadler 3 Point Notched Beam Experiments
- Asay Impact Tests
- Idar Steven’s Impact Ignition Tests

# Idar/Gray Tests Comparison

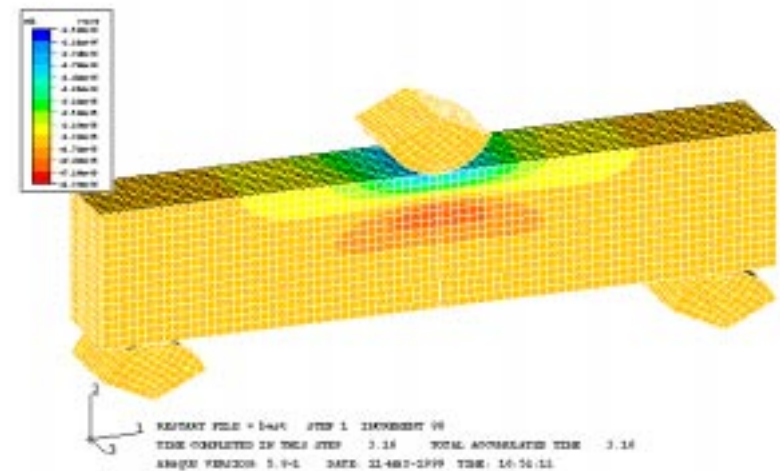
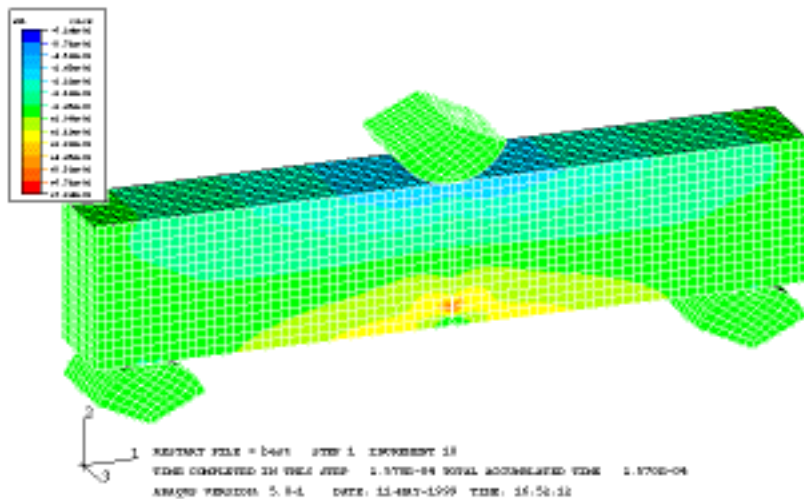




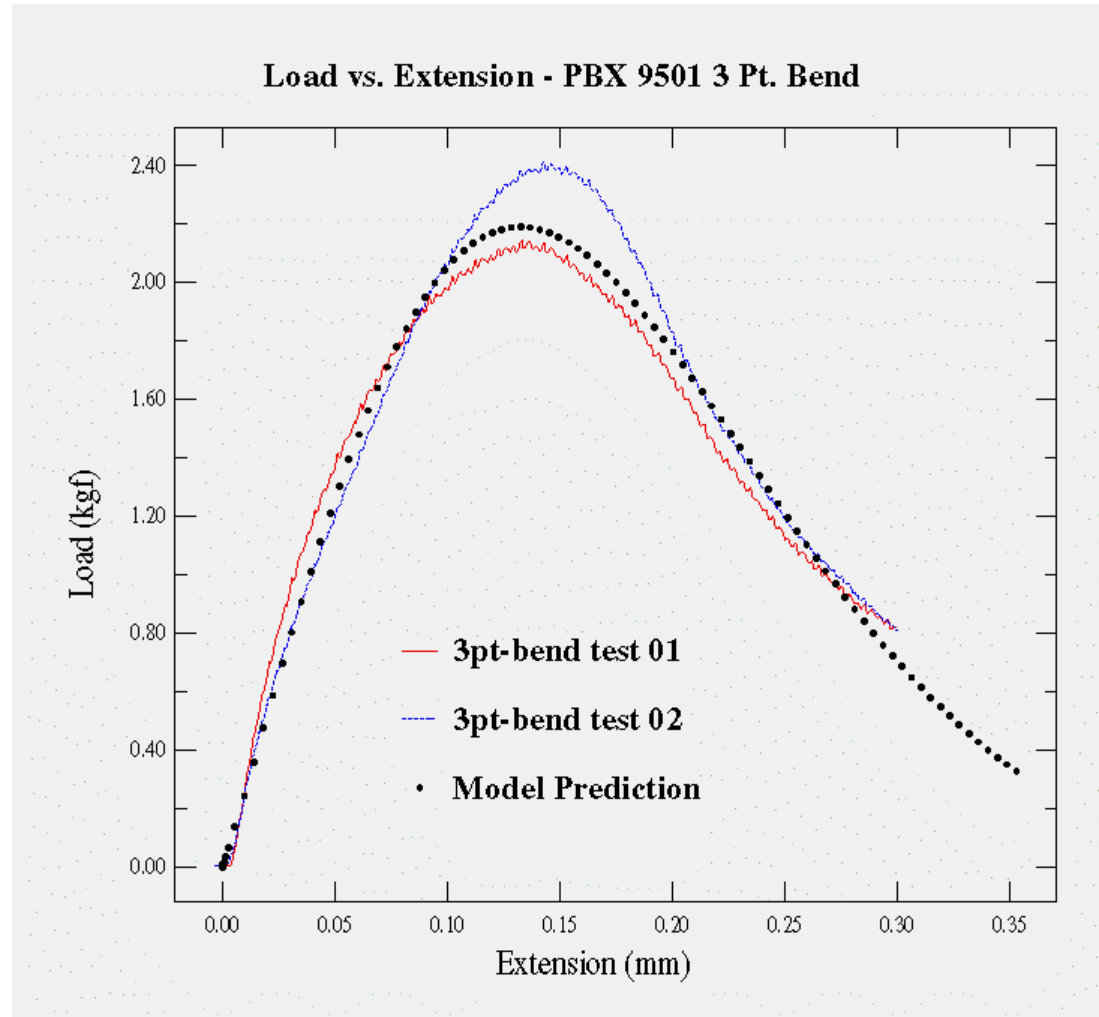
# Sadler 3-Point Beam Damage/Fracture Experiment



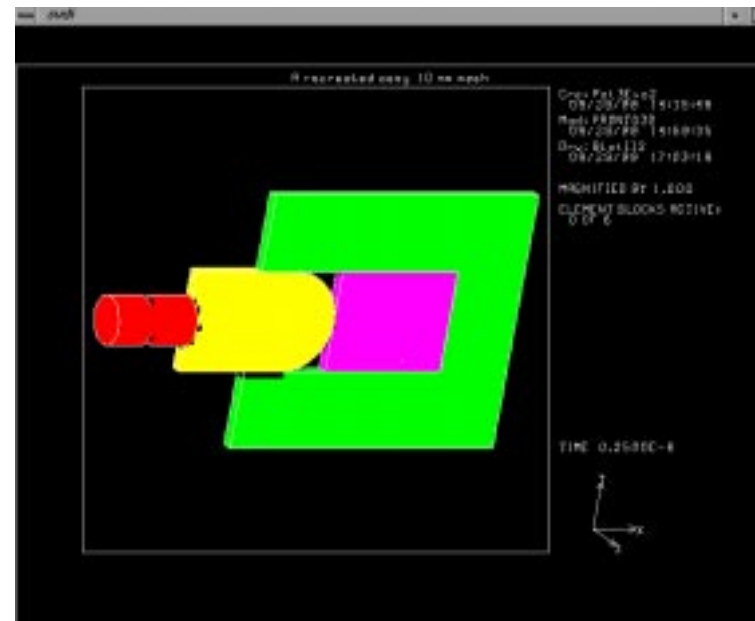
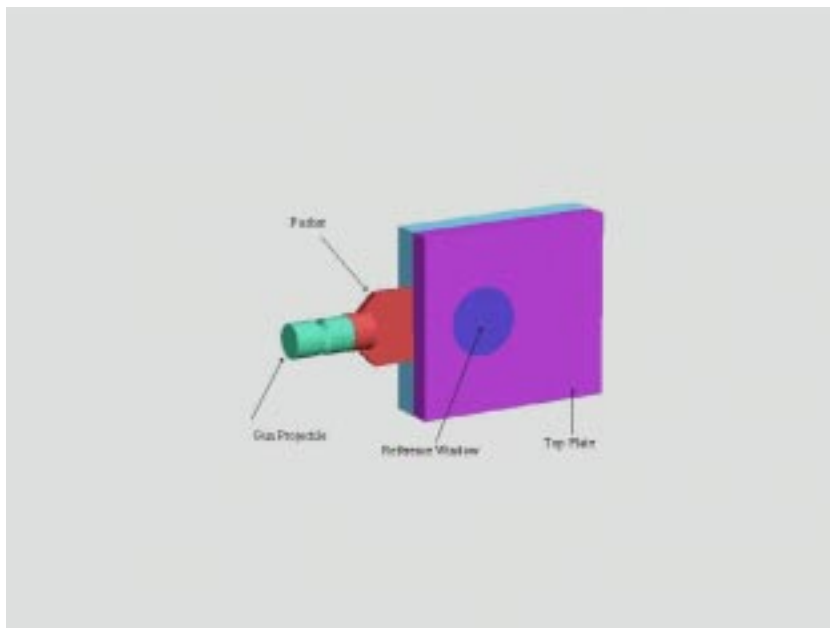
# ViscoSCRAM Damage Progression



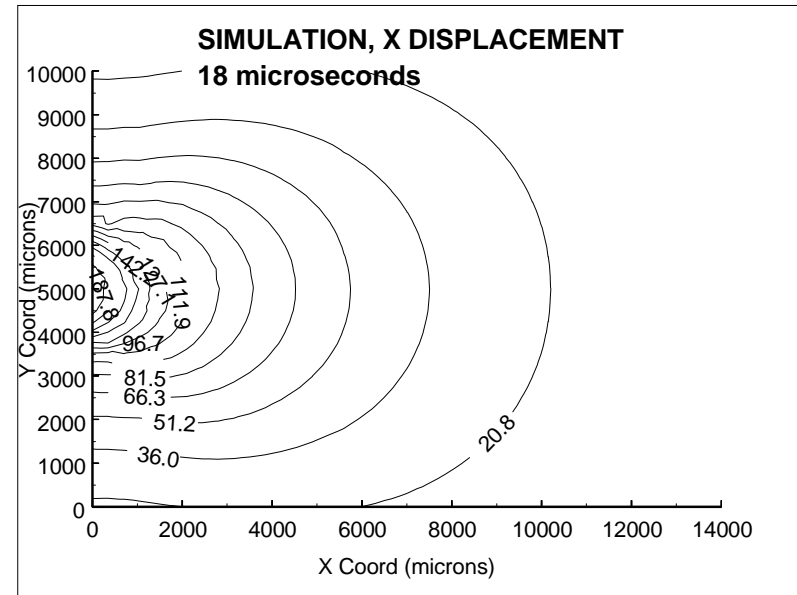
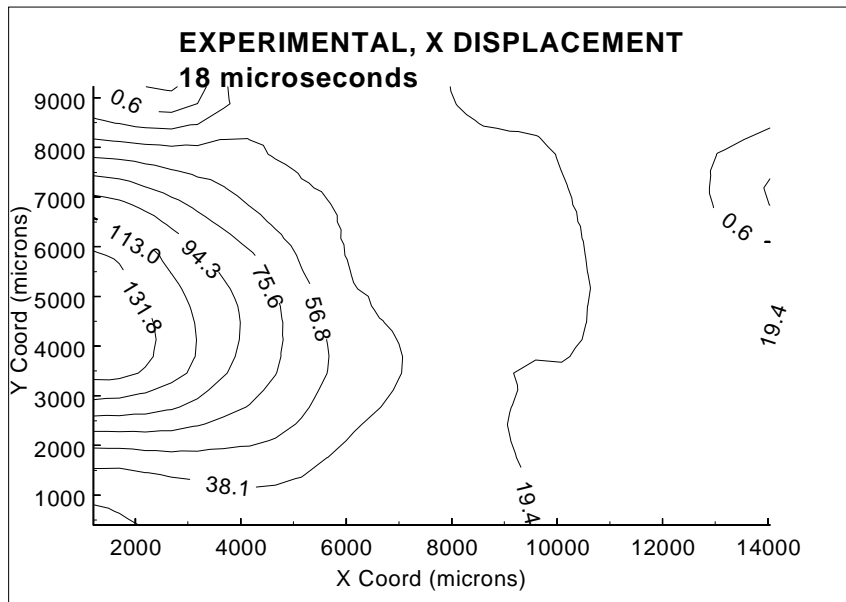
# ViscoSCRAM Comparison



# ASAY Impact Test



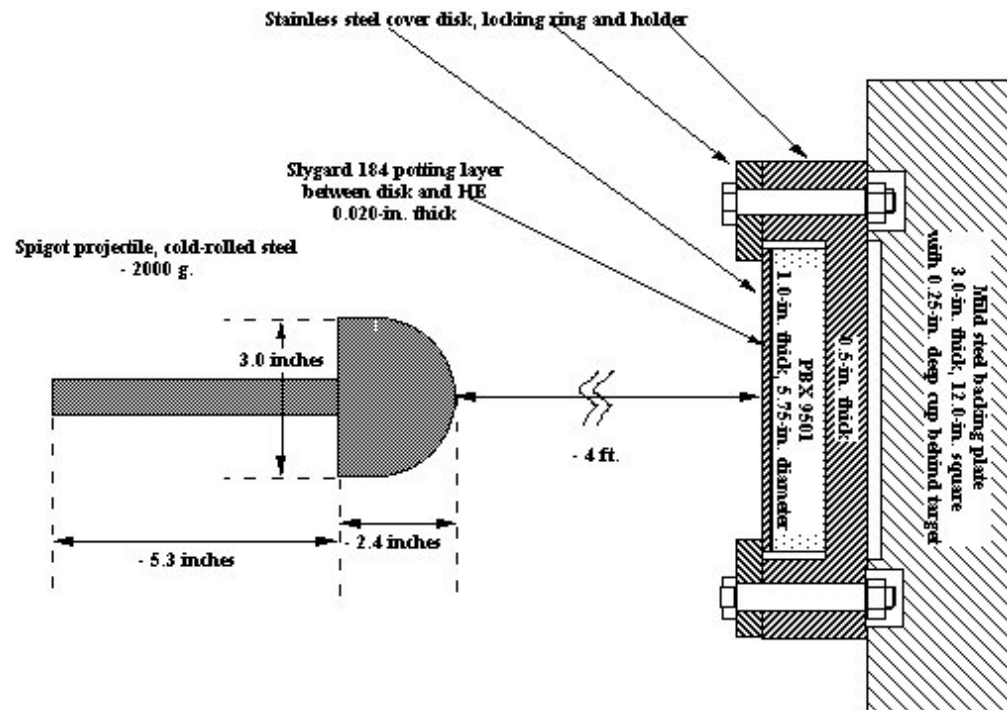
# ASAY Impact Comparison

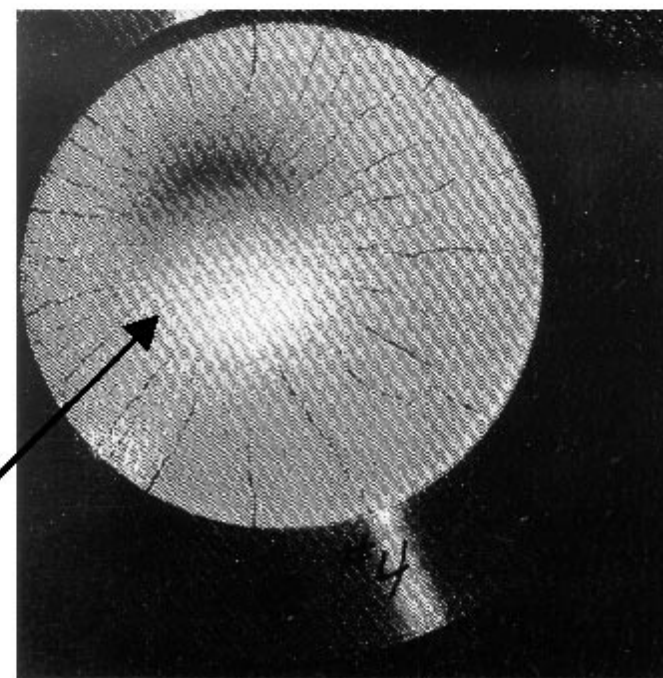
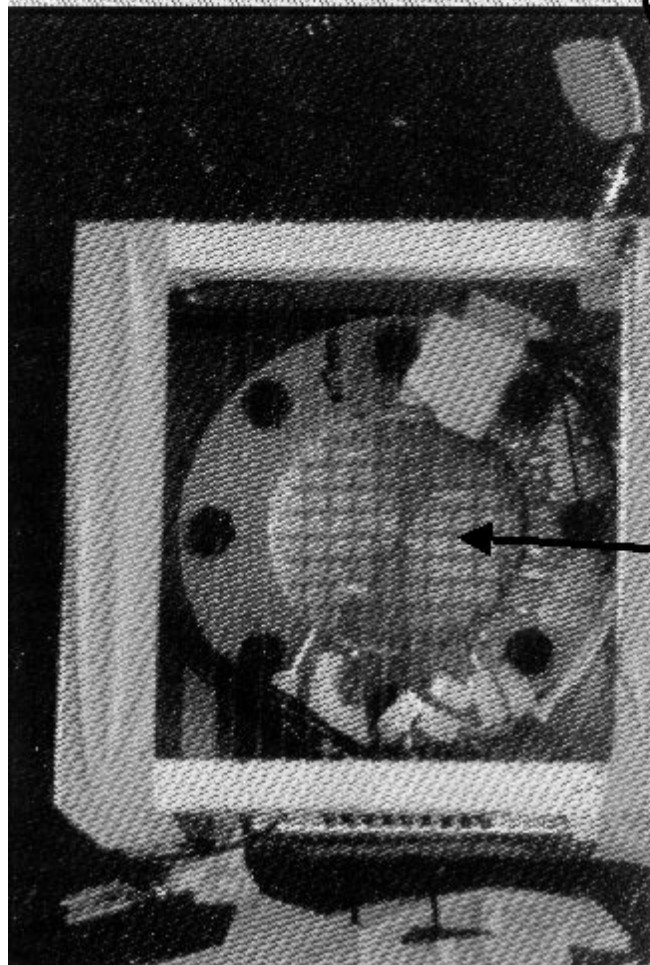
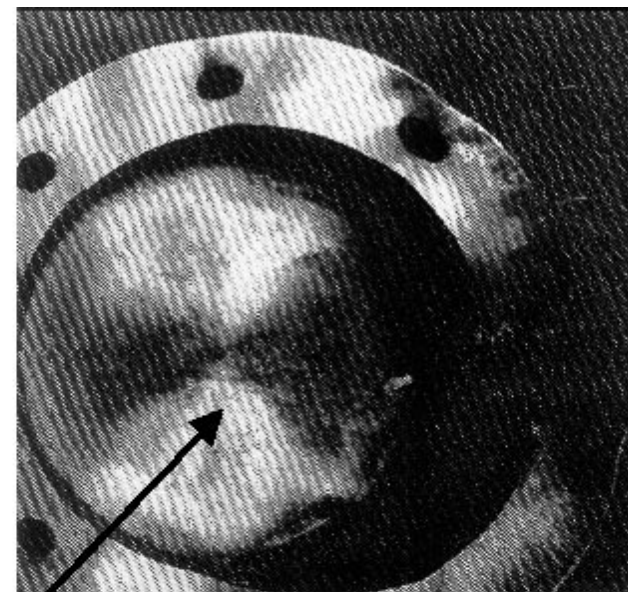
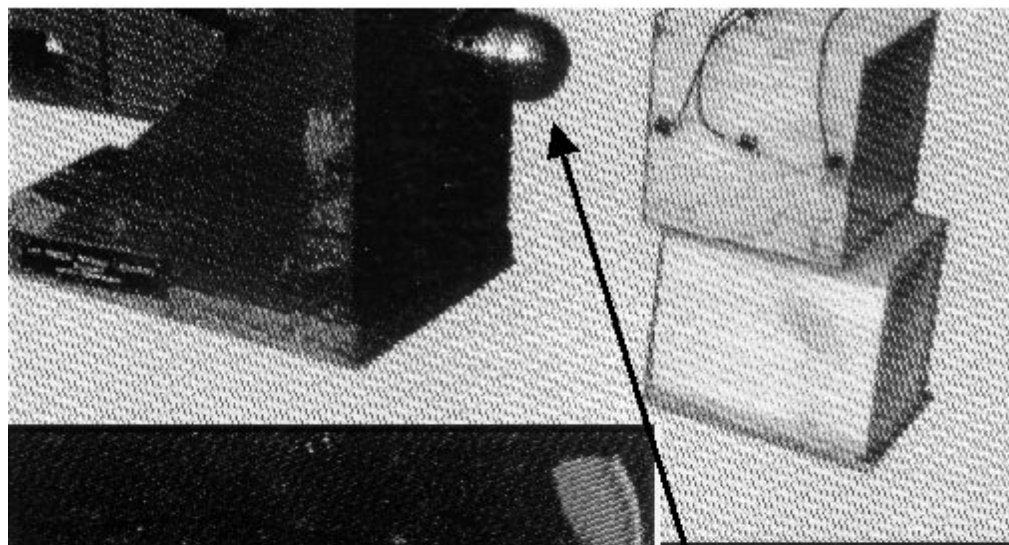


**Modeling of Idar's Spigot Gun  
(Steven's) Tests for Ignition  
Response Parameter  
Calibration are “in Progress”**

# Validation of ViscoSCRAM

- Stevens Impact Test





**Spigot Gun**

**Partial Ignition  
Test**

**Instrumented  
Specimen**

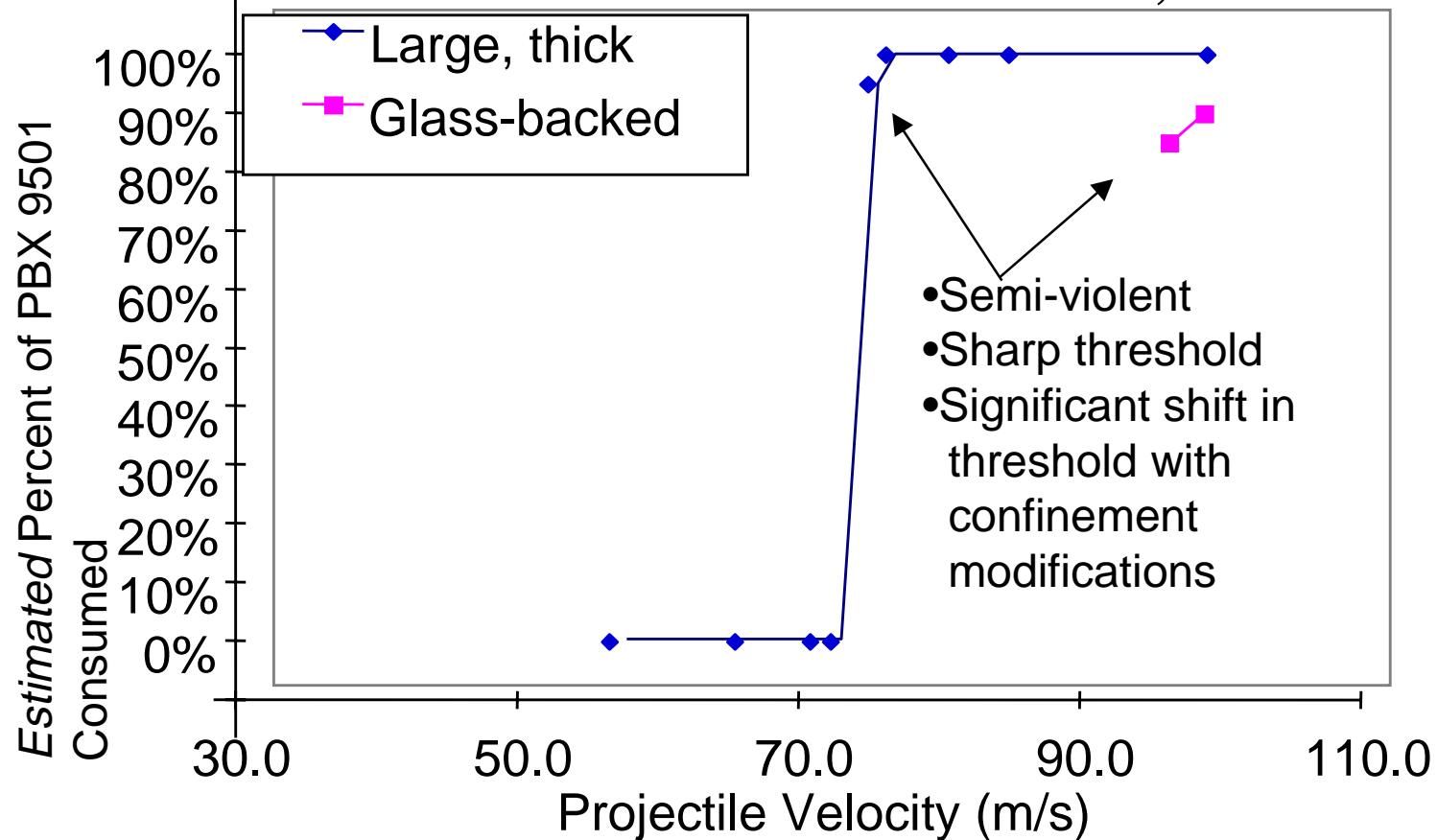
**Dented HE  
Specimen**



# Idar Steven's Ignition Test

## PBX 9501 Large, Thick Targets

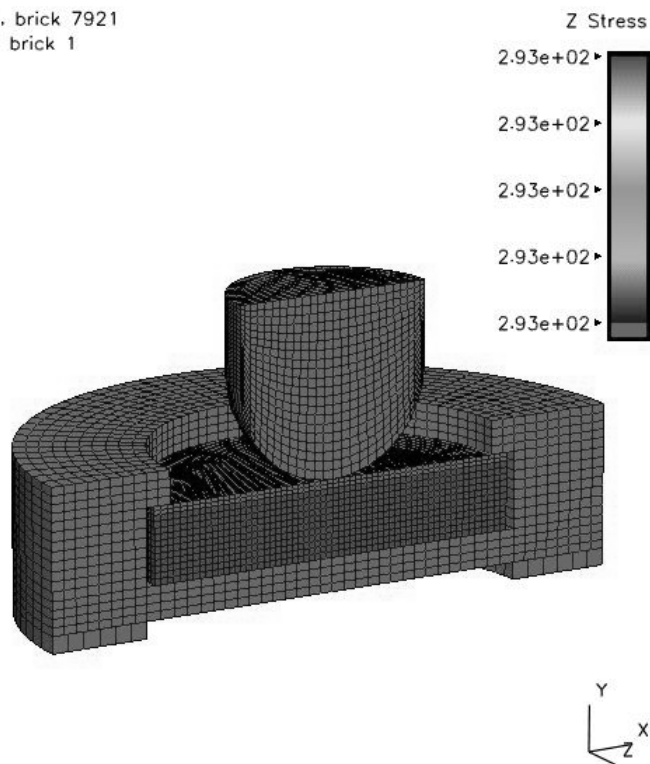
$72.2 \text{ m/s} < \text{threshold} < 75.1 \text{ m/s}$ , 1.836



# Ignition Model Calibration

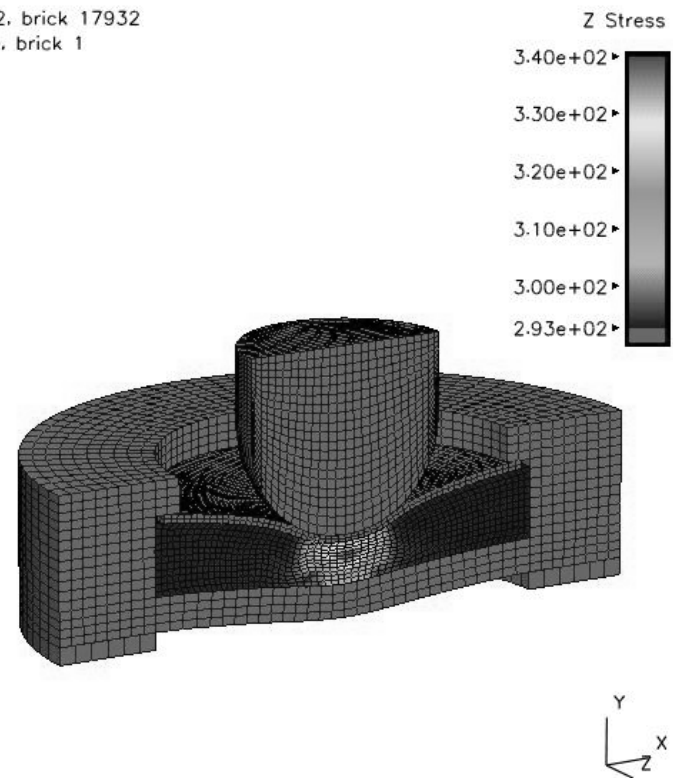
## “In Progress”

max: 2.93e+02, brick 7921  
min: 0.00e+00, brick 1



\*\* Steven Test \* Setup #2a \*  
t = 0.00000e+00

max: 3.41e+02, brick 17932  
min: 0.00e+00, brick 1



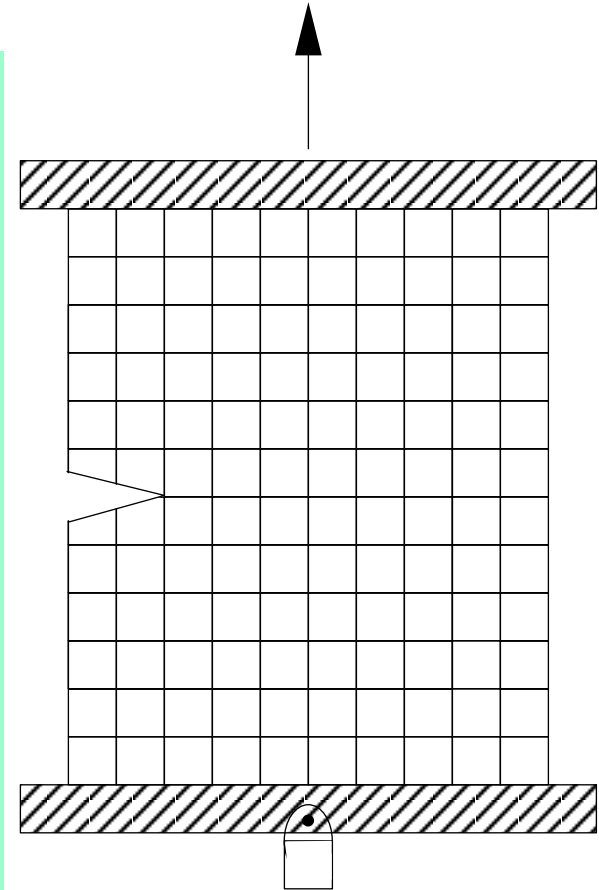
\*\* Steven Test \* Setup #2a \*  
t = 3.99966e-04

# Discrete Fracture Model Summary

- Based on the microscale-fracture modeling concepts of Alan Needleman (Brown U.), as modified to a mesoscale-fracture structural concept by Gerken/Smith/Bennett.
- Distributed randomly sized meso-scale interface fractures advance because of locally evaluated stress and material state to coalesce into finite discrete fractures.

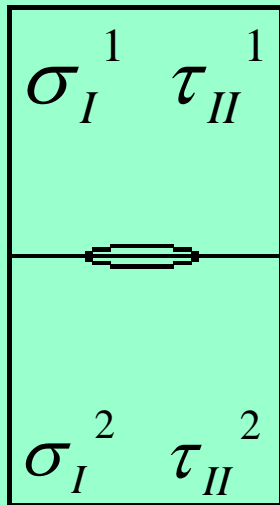
# Discrete Fracture Model

- Cracks Propagate Along Element Interfaces
- Unique Nodal Connectivity for Each Element
  - Maintain Nodal Connectivity
  - No Remeshing



# Discrete Fracture Model

- Interface Failure



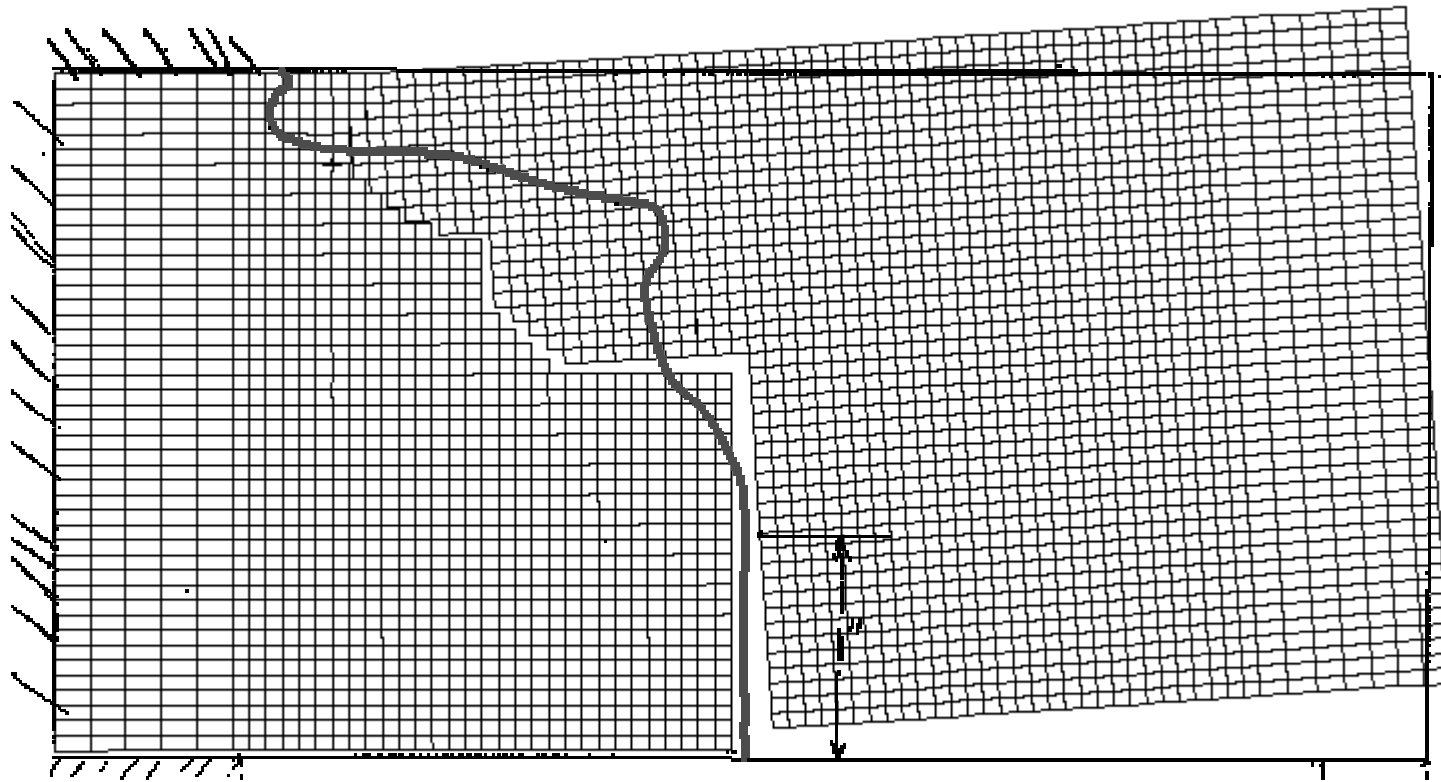
$$\sigma_I = \frac{\sigma_I^1 + \sigma_I^2}{2}$$

$$\tau_{II} = \frac{\tau_{II}^1 + \tau_{II}^2}{2}$$

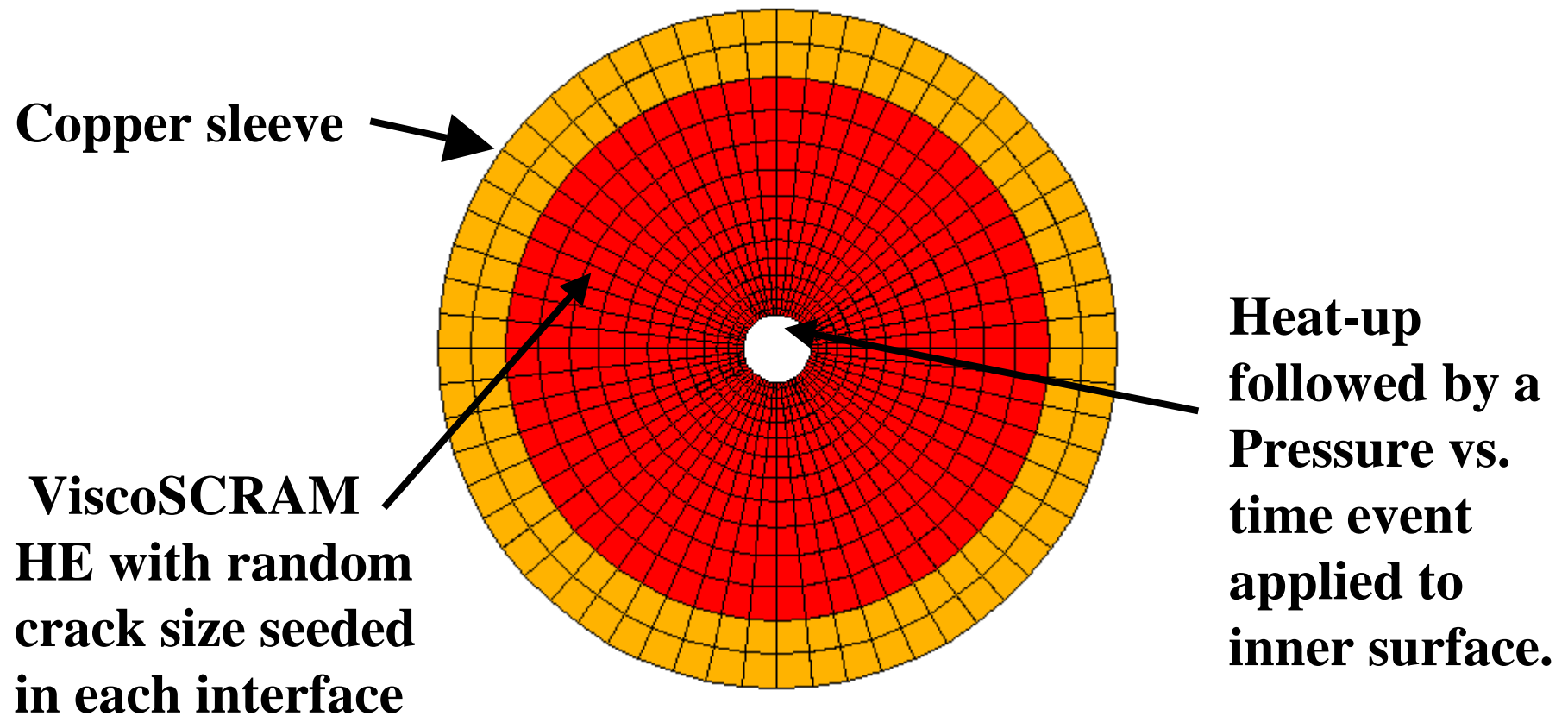
# Discrete Fracture Model Summary

- Simple in concept, but rich in Engineering Fracture Mechanics theory, and not easily implemented.
- “An Implicit Finite Element Method for Discrete Dynamic Fracture”, by Jobie M. Gerken, a Master’s Thesis in Mechanical Engineering submitted to the Colorado State University (Oct. 1998).

# Discrete Fracture Model



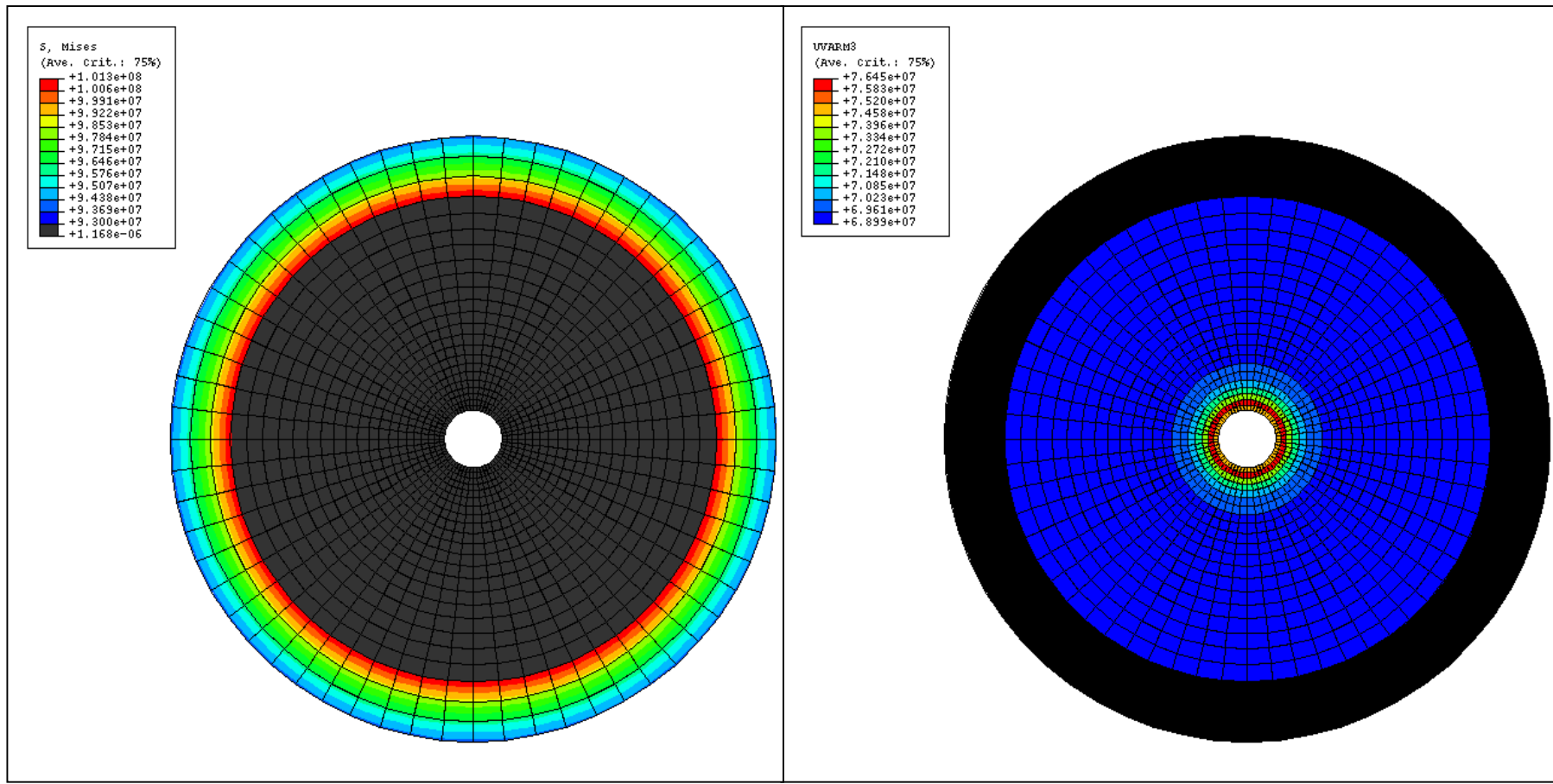
# Modeling MCCO





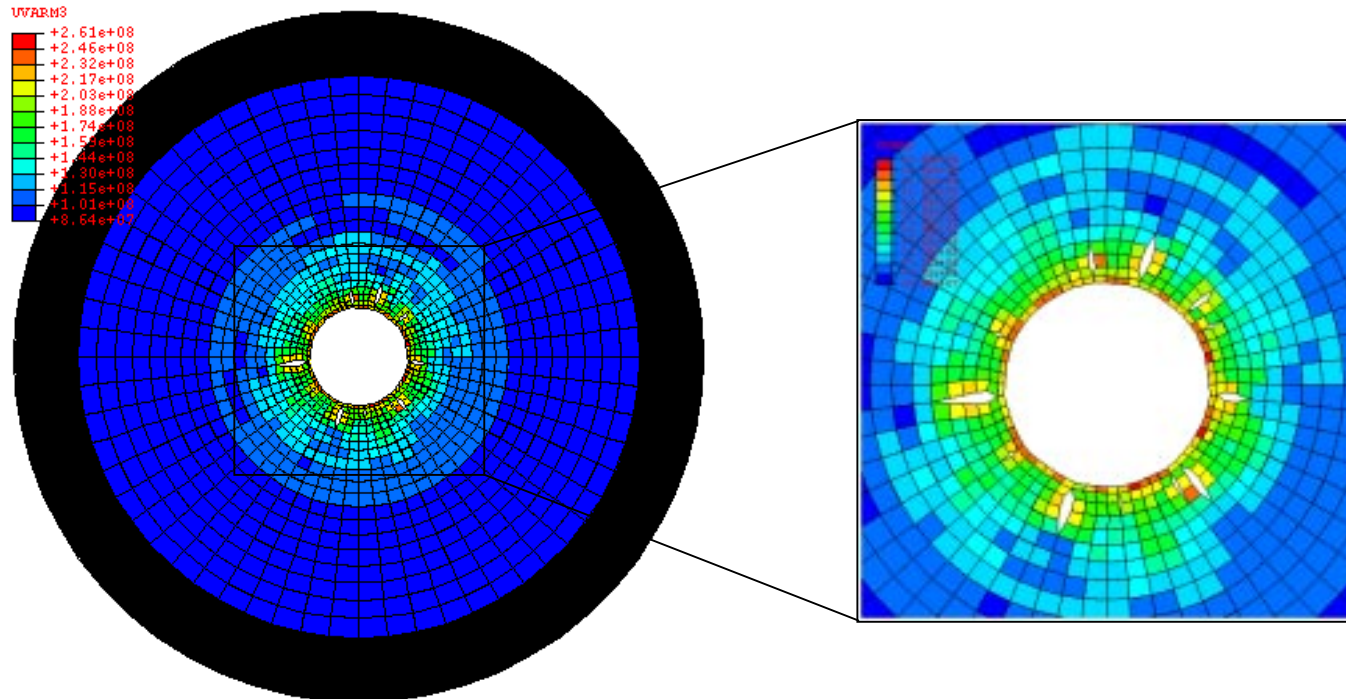
# Modeling the MCCO

- Heat Up 120 K
  - Thermal Expansion Mismatch Causes Tensile Stress in Cu and Compressive Stress in HE

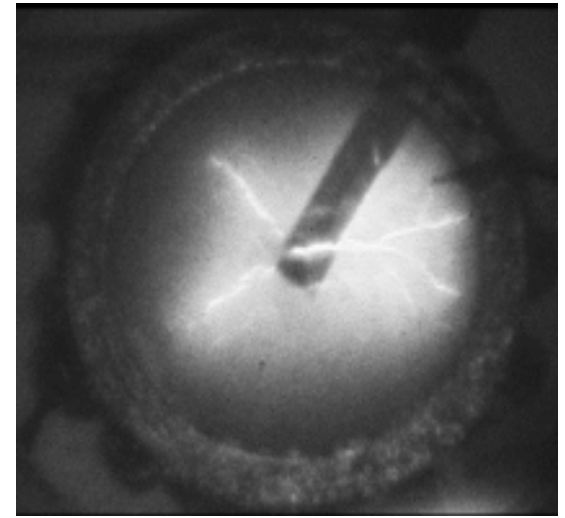


# Mechanically Coupled Cook Off

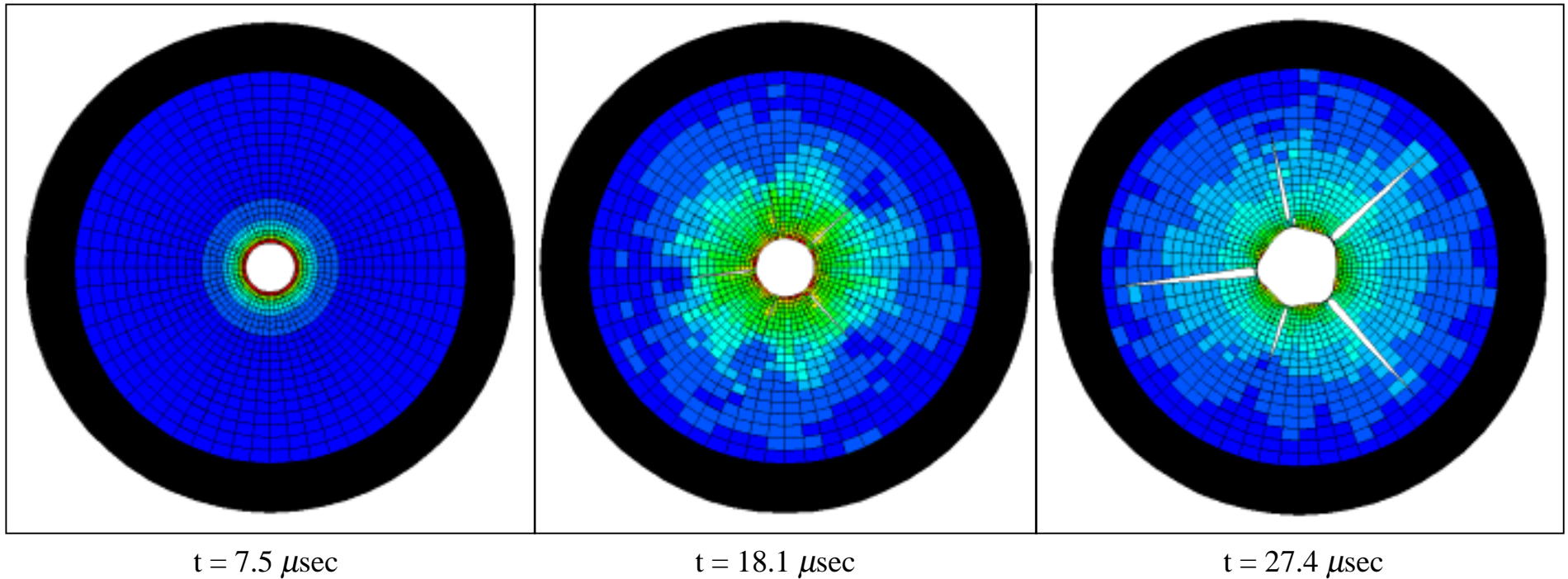
- Apply Pressure - 5MPa/ $\mu$ sec



# Modeling the MCCO

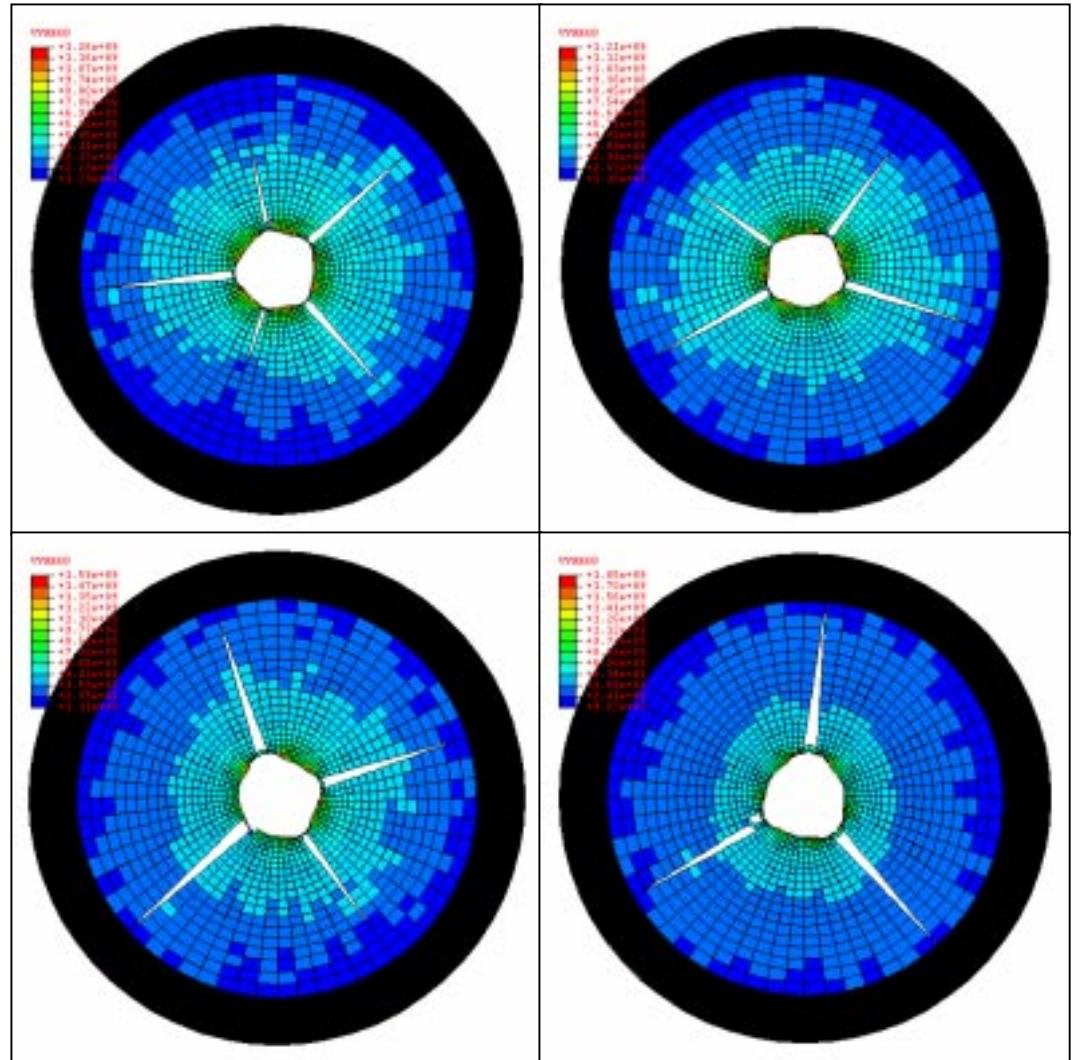


Effective Stress Contours:



# Modeling the MCCO

- Different Random Distribution Results in Different Crack Pattern
- Always 3 to 5 Large Discrete Cracks



# ViscoSCRAM and MCCO

- **ViscoSCRAM - An Engineering Material Model has been developed for ASCI STS Engineering Analysis Codes**
  - **Mechanical Validation “Complete”**
  - **Ignition Validation nearing Completion**
- **MCCO Modeling**
  - **Maturing Very Rapidly**
  - **DX Chemical Kinetics, and Steve Son’s Flame Front Propagation and Pressure Model are planned.**

## **“OUTWARD LOOK”**

**Bennett, J.G., Haberman, K.S., Johnson, J.N., Asay, B.W. and Henson, B.F. (1998) “A Constitutive Model for the Non-Shock Ignition and Mechanical Response of High Explosives”, *J. Mech. Phys. Solids*, 46, 12, 2303-22.**

**Hackett, R. M., Bennett, J. G., “An Implicit Finite Element Model for Energetic Particulate Composite Materials,” submitted to *Int. J. Num. Meth. Eng.*, LA-UR-99-3138, June, 1999.**

**Gerken, J. M., Smith, F. W., Bennett, J. G. (1999) “Numerical Simulation of the Mechanically Coupled Cook-Off Experiment” in preparation for submission to the ASME *J. Eng. Mat. and Tech.***